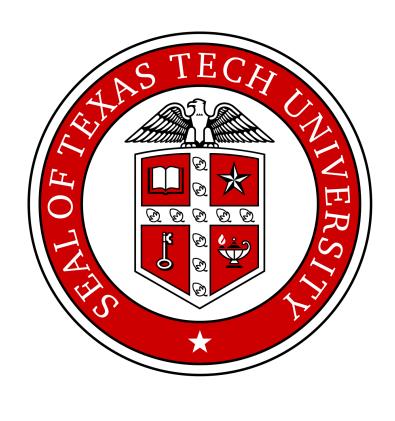
# Peaceman Model for Well-Block and Steady-State Einstein Paradigm of Brownian Motion



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## Abstract

- Used Einstein Paradigm to create model of steadystate flow to a well in circular reservoir.
- Compared this model to Peaceman's model of flow in a well-block reservoir by using Darcy's Law for rate of production q in our model and equating it to finite discrete approximation of Peaceman's rate of production q.
- Then used Forchheimer equation for non-linear model of flow, found rate of production  $\tilde{q}$  and compared it to Peaceman's q through same method.

## **Einstein Paradigm Model of Flow**

Our model of flow, where u(x, y) is "number of particles per unit volume", has this system of equations:

$$\begin{cases} \Delta u = 0\\ u|_{\partial B(0,R_e)} = P_e \\ u|_{\partial B(0,R_w)} = P_w \end{cases} \quad \Omega = B(0,R_e) \backslash B(0,R_w) \quad (1)$$

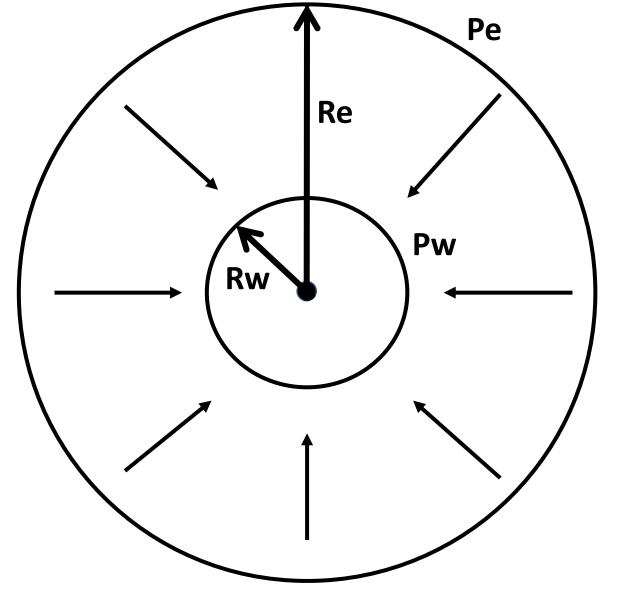
Where  $\Delta$  is the laplace. The solution u(r) of (1) is:

$$u(r) = c_1 \ln(r) + c_2$$
 (2)

With following definitions:

$$r = \sqrt{x^2 + y^2}, \ c_1 = \frac{P_e - P_w}{\ln\left(\frac{R_e}{R_w}\right)}$$
$$c_2 = \frac{P_e \ln\left(\frac{1}{R_w}\right)}{\ln\left(\frac{R_e}{R_w}\right)} + \frac{P_w \ln\left(R_e\right)}{\ln\left(\frac{R_e}{R_w}\right)}$$





## **FDA of Peaceman Model**

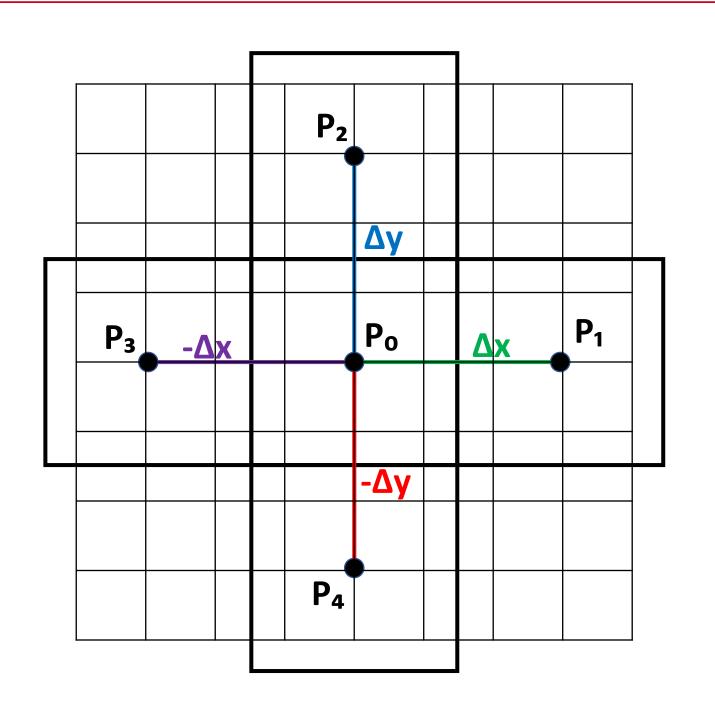
Peaceman's equation for steady-state pressure distribution:

$$q_{i,j} = \frac{kh\Delta y}{\mu\Delta x} (p_{i+1,j} - 2p_{i,j} + p_{i-1,j}) + \frac{kh\Delta x}{\mu\Delta y} (p_{i,j+1} - 2p_{i,j} + p_{i,j-1})$$

Where  $q_{i,j} = 0$  if  $i \neq 0$  or  $j \neq 0$ . We let i = 0, j = 0, h = 1, and fix  $\Delta x = \Delta y$ :

$$q = \frac{k}{\mu} \cdot \left[P_1 + P_2 + P_3 + P_4 - 4P_0\right]$$
(4)

#### **Peaceman Model on Grid**



### **Analytical vs. Discrete Formulae**

We have  $P_1 = P_2 = P_3 = P_4 = P_e$ . We then let  $P_w = P_0, R_e = \Delta$ , and  $R_w = R_0$ , for which  $R_0$  has an unknown value.

To find the value for  $R_0$ , we equate Peaceman's q to our q:

$$\frac{k}{\mu} \cdot \left[4P_e - 4P_0\right] = \frac{2\pi k}{\mu} \cdot \frac{P_e - P_0}{\ln\left(\frac{\Delta}{R_0}\right)} \tag{5}$$

Which simplifies to:

$$R_0 = \Delta x \cdot e^{-\pi/2}$$

Exactly what Peaceman derived in his paper, thus our linear steady-state model is justified.

## **Analytical Solution from Darcy Law**

The rate of production q in our model is given:

Where k is permeability,  $\mu$  is viscosity, and h is the height of the reservoir. For our calculations, we will assume  $k, \mu$  to be constants and h = 1. We simplify:



The generalized Forchheimer equation for rate of production  $\tilde{q}$  with equation of continuity  $v_r = C \frac{1}{r}$ :

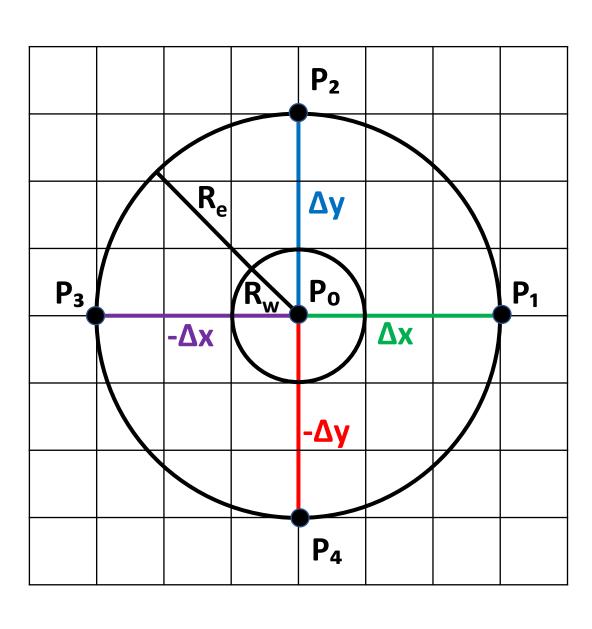
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$$q = \frac{kh}{\mu} \int_{\partial B(0, R_{\rm en})} \frac{\partial u}{\partial r} ds \tag{7}$$

$$q = \frac{2\pi k}{\mu} \cdot \frac{P_e - P_w}{\ln\left(\frac{R_e}{R_w}\right)} \tag{8}$$

#### **Circular Model on grid**



## **Forchheimer Relation for Pressure**

$$\tilde{q} = V_r \Big|_{r=R_w} \cdot 2\pi R_w \tag{9}$$

$$\tilde{q} = 2\pi \left(\frac{B - \sqrt{B^2 + 4AD}}{2A}\right)$$

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# **Forchheimer Model of Flow in Media**

From Forchheimer's equation in the radial case:

$$\begin{cases} -\frac{\partial p}{\partial r} \\ p|_{r=1} \\ p|_{r=1} \end{cases}$$

With solution:

With the following definitions and functions:

 $C_1$ 

# **Results: Forchheimer vs. Peaceman**

By equating our  $\tilde{q}$  and Peaceman's q, we can get corresponding value of  $R_w$  with fixed  $\beta$ :

$$2\pi \left(\frac{B - \sqrt{B^2 + 4AD}}{2A}\right) = \frac{k}{\mu} [4P_e - 4P_0]$$
 (14)

• Let  $R_e = \Delta$  in functions  $A(R_e, R_w)$  and  $B(R_e, R_w)$ . Let  $P_w = P_0$  in function  $D(P_e, P_w)$ 

of  $\alpha$ ,  $\beta$ ,  $P_0$ ,  $P_e$ ,  $\Delta$ .

(10)



$$\frac{\partial p}{\partial r} = \alpha v_r(r) + \beta \left( v_r(r) \right)^2 \tag{11}$$

BVP for radial P(r) in the domain with boundary conditions and equation of continuity  $v_r = C\frac{1}{r}$ :

$$= C \frac{\alpha}{r} + C^2 \beta \frac{1}{r^2}$$

$$R_w = P_w , \quad R_w < r < R_e$$
(12)
$$R_e = P_e$$

$$P(r) = -C\alpha \ln(\frac{r}{R_e}) + C^2\beta \frac{1}{r} + C_1$$
 (13)

$$C = \frac{B - \sqrt{B^2 + 4AD}}{2A}$$
$$= P_e - \left(\frac{B + \sqrt{B^2 + 4AD}}{2A}\right)\beta \frac{1}{R_e}$$
$$A(R_e, R_w) = -\beta \left(\frac{R_e - R_w}{R_e \cdot R_w}\right)$$
$$B(R_e, R_w) = \alpha \ln \left(\frac{R_e}{R_e}\right)$$
$$D(P_e, P_w) = P_e - P_w$$

•  $\alpha$  and  $\beta$  are given from the experiment.

End goal is to find  $R_w = R_0$  which will solve transcendent equation (14) with respect to known values